



Thermodynamic studies on $\text{Ba}_{2.875}\text{UO}_{5.875}(\text{s})$

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ABSTRACT

The Gibbs energy of formation of $\text{Ba}_{2.875}\text{UO}_{5.875}(\text{s})$ has been determined using manometric technique. The equilibrium $\text{CO}_2(\text{g})$ pressures over the three phase mixture: $\{\text{Ba}_{2.875}\text{UO}_{5.875}(\text{s}) + \text{Ba}_3\text{UO}_6(\text{s}) + \text{BaCO}_3(\text{s})\}$ have been measured using an absolute pressure transducer in the temperature range 1030–1220 K. The corresponding Gibbs energy expression as a function of temperature can be given as:

$$\Delta_f G_m^\circ(T)(\text{Ba}_{2.875}\text{UO}_{5.875}, \text{s}, T) \text{ (kJ mol}^{-1}\text{)} \pm 5 = -3153.1 + 0.5573 (T/\text{K})$$

$\Delta_f H_m^\circ(298.15 \text{ K})$ and $S_m^\circ(298.15 \text{ K})$ data have been calculated from the above Gibbs energy expression using required values from the literature. The corresponding values are $-3143.4 \pm 2 \text{ kJ mol}^{-1}$ and $270.8 \pm 4 \text{ J K}^{-1} \text{ mol}^{-1}$, respectively. The $\Delta_f H_m^\circ(298.15 \text{ K})$ value has also been calculated from third law method as $-3137.7 \pm 4 \text{ kJ mol}^{-1}$.

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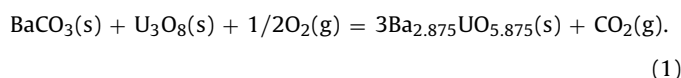
1. Introduction

Barium is an important fission product in an irradiated nuclear fuel. Thus, thermochemical stabilities of compounds in the Ba–U–O system are of importance. The stability of a compound can be calculated from its Gibbs energy of formation values. Hence, $\Delta_f G_m^\circ(T)$ of all barium uranates are required to compute the chemical form of barium in the reactor environment. Allpress [1] and Touzelin and Pialoux [2] investigated Ba–U–O system using X-ray diffraction technique. Thermodynamic functions of barium uranates are reported in the literature [3–14]. However, $\Delta_f G_m^\circ(T)$ data are limited [10,15,16]. Recently Banarjee et al. [15] have measured $\Delta_f G_m^\circ(T)$ of $\text{BaU}_2\text{O}_7(\text{s})$ and $\text{Ba}_2\text{U}_3\text{O}_{11}(\text{s})$ using e.m.f. technique. Yamawaki et al. [16] investigated the vaporization of $\text{BaUO}_3(\text{s})$ by means of Knudsen effusion mass spectrometry in the temperature range of 1770–1920 K. Matsuda et al. [10] have calculated $\Delta_f G_m^\circ(\text{BaUO}_3, \text{s}, T)$ from their heat capacity measurements and literature data. The $\Delta_f G_m^\circ(T)$ values for other uranates are not reported. In this study, the $\text{CO}_2(\text{g})$ pressure measurements have been carried out to determine $\Delta_f G_m^\circ(\text{Ba}_{2.875}\text{UO}_{5.875}, \text{s}, T)$ values using a static manometric technique in the temperature range 1030–1220 K.

2. Experimental

2.1. Material preparation

$\text{Ba}_{2.875}\text{UO}_{5.875}(\text{s})$ was prepared by the solid state reaction of $\text{BaCO}_3(\text{s})$ (0.997 mass fraction, B.D.H, UK) with $\text{U}_3\text{O}_8(\text{s})$ (0.9999 mass fraction purity, Nuclear Fuel Complex, Hyderabad, India) in the presence of air. $\text{BaCO}_3(\text{s})$ and $\text{U}_3\text{O}_8(\text{s})$ were mixed thoroughly in the ratio of 8.625:1 and calcined at 1273 K for 300 h in an alumina boat with intermediate grindings. $\text{Ba}_{2.875}\text{UO}_{5.875}(\text{s})$ has been formed due to following reaction:



The resulting reddish-orange coloured compound was characterized as $\text{Ba}_{2.875}\text{UO}_{5.875}(\text{s})$ by X-ray diffraction (XRD). The XRD pattern was taken on a STOE X-ray diffractometer, Germany, using Ni filtered $\text{Cu K}\alpha$ radiation. The X-ray diffraction (XRD) pattern shown in Fig. 1 agreed well with that reported in the literature [17,18]. Griffiths and Kemmler [17] found this compound besides $\text{Ba}_3\text{UO}_6(\text{s})$ in the BaO– UO_3 system.

A three phase mixture: $\{\text{Ba}_{2.875}\text{UO}_{5.875}(\text{s}) + \text{Ba}_3\text{UO}_6(\text{s}) + \text{BaCO}_3(\text{s})\}$ was prepared under dry condition and made into pellets under a pressure of 100 MPa. The pellets were dried and stored in a desiccator for manometric measurements.

2.2. Equilibrium technique

An all-metal ultra-high vacuum system similar to that employed earlier [19] was used to measure $\text{CO}_2(\text{g})$ pressures. The assem-

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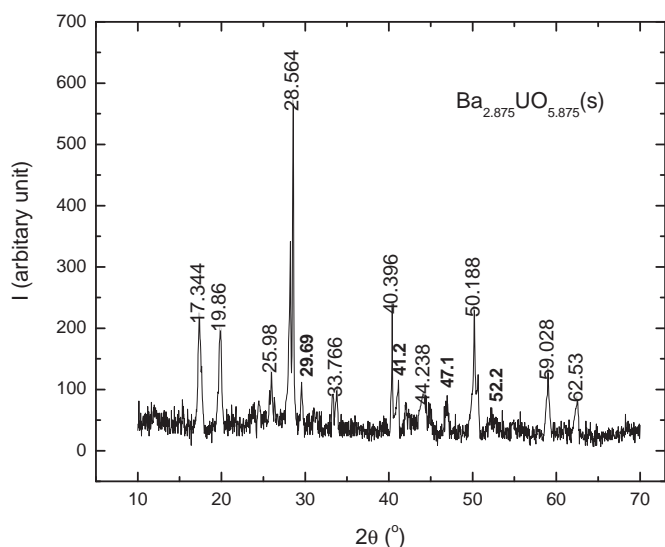


Fig. 1. X-ray diffraction pattern of $\text{Ba}_{2.875}\text{UO}_{5.875}(\text{s})$. The intensity, I (arbitrary unit) of peaks are plotted in y axis and the diffraction angle 2θ ($^\circ$) in x-axis.

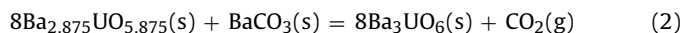
bly was evacuated and tested for leak tightness for 400 h before actual pressure measurements. The pellets of ternary mixture $\{\text{Ba}_{2.875}\text{UO}_{5.875}(\text{s}) + \text{Ba}_3\text{UO}_6(\text{s}) + \text{BaCO}_3(\text{s})\}$ were placed in an alumina boat and loaded into the quartz reaction tube, which was attached to the vacuum system. The sample was heated by a Kanthal wire-wound furnace and the temperature of the sample was maintained within $\pm 1\text{K}$ and was measured using a pre-calibrated chromel-to-alumel thermocouple. Before measuring the $\text{CO}_2(\text{g})$ pressures, the pellets were annealed under vacuum at an oxygen partial pressure of 10^{-5} kPa at 500K for 400 h.

The $\text{CO}_2(\text{g})$ pressures were measured by a absolute pressure transducer supplied by Edwards, USA. The accuracy of the transducer was $\pm 0.25\%$ of the reading. This transducer was calibrated by measuring oxygen pressure over two phase mixture: $\{\text{Cu}_2\text{O}(\text{s}) + \text{CuO}(\text{s})\}$.

The attainment of equilibrium $p(\text{CO}_2)$ over $\{\text{Ba}_{2.875}\text{UO}_{5.875}(\text{s}) + \text{Ba}_3\text{UO}_6(\text{s}) + \text{BaCO}_3(\text{s})\}$ was checked by evacuating some $\text{CO}_2(\text{g})$ and allowing the equilibrium to be attained again. An equilibrium time of 200–400 h was generally required for each experimental temperature. The X-ray diffraction pattern shown in Fig. 2 was taken after the experiment. It did not show any new peaks which is a proof of absence of any solid phases other than participating in reaction (2). This observation confirmed co-existence of the three phase mixture: $\{\text{Ba}_{2.875}\text{UO}_{5.875}(\text{s}) + \text{Ba}_3\text{UO}_6(\text{s}) + \text{BaCO}_3(\text{s})\}$.

3. Results

The $\text{CO}_2(\text{g})$ pressures generated due to the reaction:



The variation of $p(\text{CO}_2, \text{g})$ at various temperatures is given in Table 1 and shown in Fig. 3 and can be represented by the following least squares expression:

$$\{\ln p(\text{CO}_2, \text{g})/\text{kPa}\} \pm 0.05 = 12.278 - 12787 \quad (\text{K}/T). \quad (3)$$

The $\Delta_r G_m^\circ(T)$ for the reaction (2) can be given as:

$$\begin{aligned} \Delta_r G_m^\circ(T) &= -RT \ln p(\text{CO}_2, \text{g}) = 8 \Delta_f G_m^\circ(\text{Ba}_3\text{UO}_6, \text{s}, T) \\ &+ \Delta_f G_m^\circ(\text{CO}_2, \text{g}, T) - 8 \Delta_f G_m^\circ(\text{Ba}_{2.875}\text{UO}_{5.875}, \text{s}, T) \\ &- \Delta_f G_m^\circ(\text{BaCO}_3, \text{s}, T) \end{aligned} \quad (4)$$

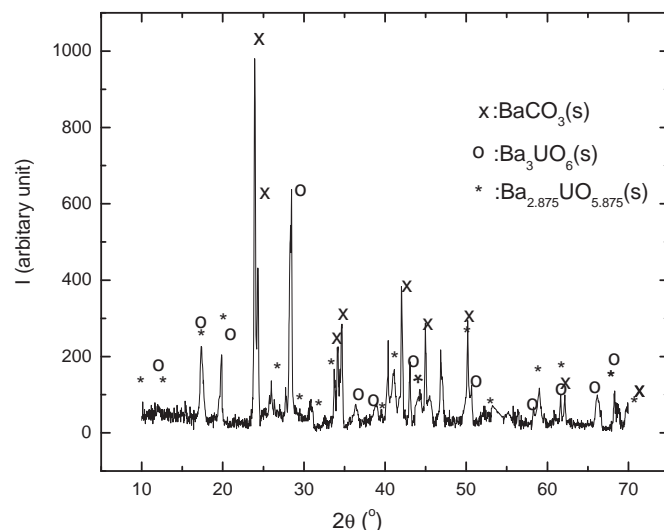


Fig. 2. X-ray diffraction pattern of the mixture: $\{\text{BaCO}_3(\text{s}) + \text{Ba}_3\text{UO}_6(\text{s}) + \text{Ba}_{2.875}\text{UO}_{5.875}(\text{s})\}$ after the experiment). The XRD peaks of $\text{BaCO}_3(\text{s})$, $\text{Ba}_3\text{UO}_6(\text{s})$ and $\text{Ba}_{2.875}\text{UO}_{5.875}(\text{s})$ are shown with different symbols.

Table 1

Equilibrium $\text{CO}_2(\text{g})$ pressures at different temperatures over the three phase mixture: $\{\text{Ba}_{2.875}\text{UO}_{5.875}(\text{s}) + \text{Ba}_3\text{UO}_6(\text{s}) + \text{BaCO}_3(\text{s})\}$.

T (K)	$10 \cdot p(\text{CO}_2, \text{g})$ (kPa)	T/K	$10 \cdot p(\text{CO}_2, \text{g})$ (kPa)
1030	8.65 ± 0.02	1110	22.8 ± 0.06
1040	9.32 ± 0.02	1120	24.2 ± 0.07
1060	12.0 ± 0.03	1140	28.71 ± 0.09
1070	14.4 ± 0.04	1157	35.16 ± 0.10
1071	13.3 ± 0.03	1168	37.48 ± 0.12
1080	15.8 ± 0.04	1178	39.91 ± 0.11
1090	17.0 ± 0.07	1191	48.85 ± 0.12
1100	19.8 ± 0.09	1220	55.96 ± 0.14

The $\Delta_r G_m^\circ(T)$ can be calculated from Eqs. (4) and (3) and are given as:

$$\begin{aligned} \{\Delta_r G_m^\circ(T) (\text{kJ mol}^{-1})\} \pm 0.3 &= 106.3 - 0.0637 \quad (T/\text{K}) \\ &\times (1030 \leq T/\text{K} \leq 1220) \end{aligned} \quad (5)$$

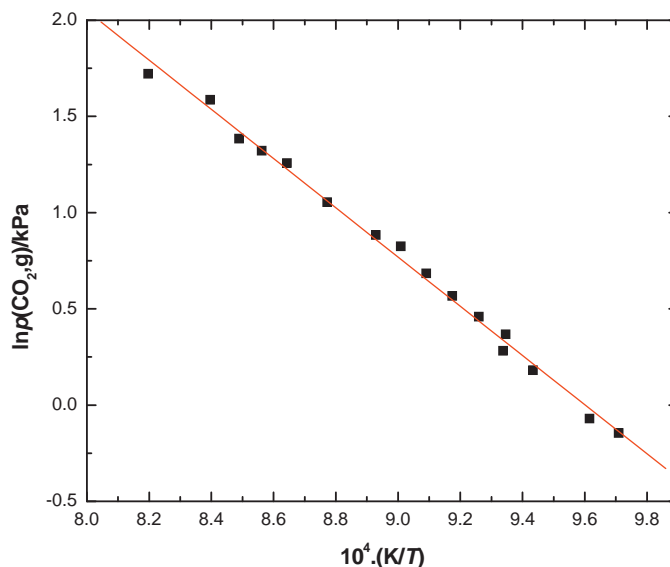


Fig. 3. Temperature dependence of equilibrium vapour pressure of $\text{CO}_2(\text{g})$ over phase mixture: $\{\text{Ba}_{2.875}\text{UO}_{5.875}(\text{s}) + \text{Ba}_3\text{UO}_6(\text{s}) + \text{BaCO}_3(\text{s})\}$.

The $\Delta_f G_m^\circ(\text{Ba}_{2.875}\text{UO}_{5.875}, s, T)$ has been computed using Eq. (5) and $\Delta_f G_m^\circ(T)$ values for $\text{BaCO}_3(s)$ [20] and $\text{CO}_2(g)$ [21] from Eqs. (6) and (7)

$$\Delta_f G^\circ(\text{BaCO}_3, s, T) \text{ (kJ mol}^{-1}\text{)} = -1194.7 + 0.2403 (T/K), \quad (6)$$

$$\Delta_f G^\circ(\text{CO}_2, g, T) \text{ (kJ mol}^{-1}\text{)} = -394.8 - 0.00108 (T/K), \quad (7)$$

and that for $\text{Ba}_3\text{UO}_6(s)$ from Table 2. The corresponding $\Delta_f G_m^\circ(\text{Ba}_{2.875}\text{UO}_{5.875}, s, T)$ expression can be given as:

$$\Delta_f G_m^\circ(\text{Ba}_{2.875}\text{UO}_{5.875}, s, T) (\pm 5 \text{ kJ mol}^{-1}) = -3153.1 + 0.5573 \times (T/K) \quad (1030 \leq T/K \leq 1220) \quad (8)$$

The intercept and slope of above Gibbs energy expression gives enthalpy of formation and entropy of $\text{Ba}_{2.875}\text{UO}_{5.875}(s)$ at 1125 K, experimental average temperature. Using heat capacity values from our studies [22], enthalpy and entropy of transitions of barium from JANAF tables [21] and uranium from CODATA [23], $\Delta_f H_m^\circ(298.15 \text{ K})$ and $S_m^\circ(298.15 \text{ K})$ have been calculated from second law method. The corresponding values are $-3143.4 \pm 2 \text{ kJ mol}^{-1}$ and $270.8 \pm 4 \text{ J K}^{-1} \text{ mol}^{-1}$. The $\Delta_f H_m^\circ(298.15 \text{ K})$ values were also calculated by the third law method for each experimental points using Gibbs energy functions: $\phi_m^\circ = \{(G_m^\circ(T) - H_m^\circ(298.15 \text{ K}))/T\}$ for $\text{Ba}_{2.875}\text{UO}_{5.875}(s)$ and $\text{Ba}_3\text{UO}_6(s)$ from our previous study [22] and that for $\text{BaCO}_3(s)$ and $\text{CO}_2(g)$ from the literature [20,21]. This value is $-3137.7 \pm 4 \text{ kJ mol}^{-1}$ which, is selected as $\Delta_f H_m^\circ(\text{Ba}_{2.875}\text{UO}_{5.875}, s, 298.15 \text{ K})$.

4. Discussion

Experimental Gibbs energy data on $\text{Ba}_{2.875}\text{UO}_{5.875}(s)$ have not been reported in the literature. However, present authors [22] have calculated it from the heat capacity and literature data. This expression is included in Table 2 for comparisons. $\Delta_f G_m^\circ(1100 \text{ K})$ calculated from Ref. [22] ($-2545.6 \text{ kJ mol}^{-1}$) and this study ($-2540.1 \pm 5 \text{ kJ mol}^{-1}$) matches well. $\Delta_f G_m^\circ(T)$ values for $\text{Ba}_3\text{UO}_6(s)$ [22] and $\text{BaUO}_4(s)$ [11,20] have been fitted into expression and are included in Table 2. $\Delta_f G_m^\circ(T)$ values for $\text{Ba}_2\text{U}_3\text{O}_{11}(s)$ and $\text{BaU}_2\text{O}_7(s)$ reported in our previous study [15] have also been given in Table 2. Heat capacity expressions and $S_m^\circ(298.15 \text{ K})$ data reported for Ba-U-O system [11,20,22,24] are also included in Table 2.

The $\Delta_f G_m^\circ(T)/g$ of $\text{Ba}_3\text{UO}_6(s)$, $\text{Ba}_{2.875}\text{UO}_{5.875}(s)$, $\text{BaUO}_4(s)$, $\text{BaU}_2\text{O}_7(s)$ and $\text{Ba}_2\text{U}_3\text{O}_{11}(s)$ have been plotted as a function of temperature in Fig. 4. It shows that, in the sixth oxidation state of uranium, $\text{Ba}_3\text{UO}_6(s)$ is the most stable and $\text{BaU}_2\text{O}_7(s)$ as least stable barium uranate. It leads to the conclusion that addition of $\text{BaO}(s)$ into $\text{BaUO}_4(s)$ increases its stability more than the addition of $\text{UO}_3(s)$ into $\text{BaUO}_4(s)$.

Fig. 5 gives the plot of enthalpy of formations of $\text{Ba}_x\text{U}_y\text{O}_{x+3y}(s)$ (hexa valent barium uranates, given in Table 2) as a function of atomic weight. It shows a regular decrease in $\Delta_f H_m^\circ(298.15 \text{ K})$ with increase in atomic weight. The enthalpy of formation of $\text{Ba}_x\text{U}_y\text{O}_{x+3y}(s)$ can be calculated from the following expression:

$$\Delta_f H_m^\circ(\text{Ba}_x\text{U}_y\text{O}_{x+3y}, s, 298.15 \text{ K}) (\pm 1\%) \text{ kJ mol}^{-1} = -684.43x - 1252.518y + 62.9y/(x - 2y), \quad (9)$$

where x and y are the number of barium and uranium atoms in $\text{Ba}_x\text{U}_y\text{O}_{x+3y}(s)$. When $\Delta_f H_m^\circ(298.15 \text{ K})/g$ values of hexa-valent barium uranates are plotted against Ba/U mole ratio, two different lines with opposite slope are obtained which are shown in Fig. 6. The $\Delta_f H_m^\circ(298.15 \text{ K})/g$ of $\text{Ba}_2\text{U}_3\text{O}_{11}(s)$ [11] $\text{BaU}_2\text{O}_7(s)$ [24] and $\text{BaUO}_4(s)$ [25] fall in one series and $\text{BaUO}_4(s)$ [25], $\text{Ba}_{2.875}\text{UO}_{5.875}(s)$ and

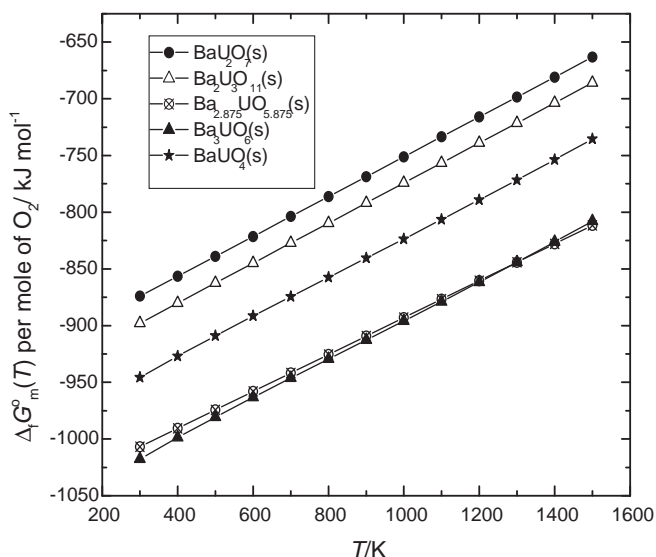


Fig. 4. The standard molar Gibbs energy of formation of barium uranates in BaO-UO₃ system.

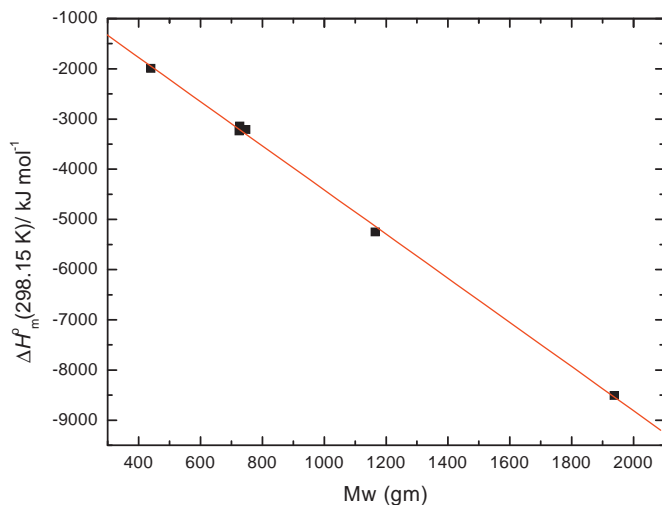


Fig. 5. The plot of $\Delta_f H_m^\circ(298.15 \text{ K})$ versus temperature for barium uranates in BaO-UO₃ system.

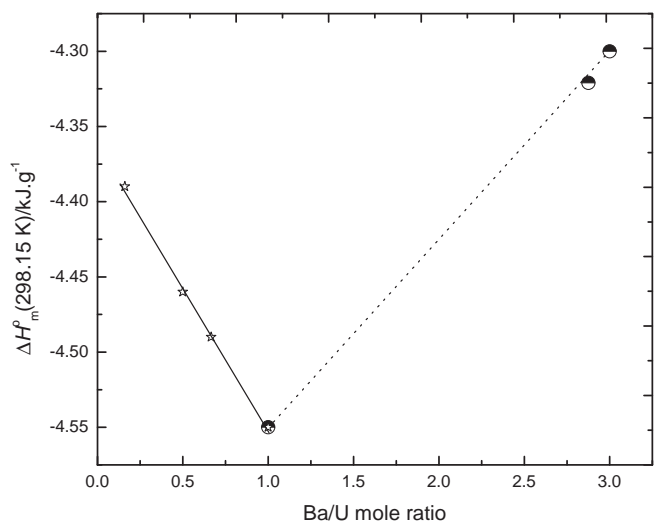


Fig. 6. The plot of $\Delta_f H_m^\circ(298.15 \text{ K})/g$ versus Ba/U mole ratio for barium uranates in BaO-UO₃ system.

Table 2

Thermodynamic functions for compounds in Ba-U-O system. Gibbs energy is expressed as: $\Delta_f G_m^{\circ}(T)/\text{kJ mol}^{-1} = A + B (T/\text{K})$ and molar heat capacity is expressed as: $C_{p,m}^{\circ}(T)/\text{J K}^{-1} \text{ mol}^{-1} = a + b(T/\text{K}) + c(\text{K}/T)^2$.

Compounds	Method	Temperature range T/K	$\Delta_f G_m^{\circ}(T)/\text{kJ mol}^{-1}$		$\Delta_f H_m^{\circ}(298.15\text{K})/\text{kJ mol}^{-1}$	$S_m^{\circ}(298.15\text{K})/\text{J K}^{-1} \text{ mol}^{-1}$	$C_{p,m}^{\circ}(T)/\text{J K}^{-1} \text{ mol}^{-1} = a + b(T/\text{K}) + c(\text{K}/T)^2$		
			A	B			a	$b \times 10^3$	$c \times 10^{-5}$
BaUO ₃ (s) [9,10,16,24]	KEMS [16]	1770–1920	–	–	–1742.5 ± 1.7	–	–	–	–
	E.m.f. [26]	1060–1090	–	–	–	–	–	–	–
	DSC [10]	373–873	–1722.7 ^a	0.2709	–	142	126.6	16.1	–1.42
Ba ₂ U ₂ O ₇ (s) [7,24]	SC [9]	–	–	–	–1690 ± 10 [24]	–	–	–	–
	SC [7]	–	–	–	–3740.0 ± 6.3 [24]	296 ± 15 [24]	–	–	–
	SC [25]	–	–	–	–1993.8 ± 3.3 [24]	154.0 ± 2.5 [24]	–	–	–
BaUO ₄ (s) [11,19,24,25]	C [20]	–	–1994.8 ^b	0.3476	–	–	153.781 ^b	9.179	–27.778
	–	–	–	–	–	–	–	–	–
BaU ₂ O ₇ (s) [7,15,22,24]	E.m.f. [15]	1001–1206	–3243.8	0.6148	–	–	–	–	–
	SC [7]	–	–	–	–3237.2 ± 5 [24]	260 ± 15 [24]	–	–	–
	CV [22]	299–1000	–3239.2	0.6154	–	260.7 ± 4	214.51	61.254	–37.665
Ba ₂ U ₃ O ₁₁ (s) [11,15,22]	E.m.f. [15]	1009–1178.5	–5229.3	0.9709	–5237.2	–	–	–	–
	E [11]	–	–	–	–5250 ± 25 [11]	405 ± 5 [11]	–	–	–
	CV [22]	323–1000	–5235.8	0.9755	–	411.2 ± 4	396.4	31.094	70.966
BaU _{6,42} O _{19,7} (s) [32]	E [32]	–	–	–	–8509.6	–	–	–	–
Ba ₃ UO ₆ (s) [7,11,22,24]	SC [7]	–	–	–	–3210.4 ± 8 [24]	298 ± 15 [24]	–	–	–
	CV [22]	302–1012	–3239.8 ^c	0.5795	–	296.5 ± 4	307.12	7.4788	–82.742
Ba _{2,875} UO _{5,875} (s) [22]	CV [22]	306–1011	–	–	–	281.7 ± 4	287.64	9.498	–67.054
	E	900–1200	–3137.0 ^c	0.5378	–	–	–	–	–
Present study	M	1030–1220	–3153.1	0.5573	3137.3 ± 4	270.8 ± 4	–	–	–

KEMS = Knudsen effusion mass-spectrometry, E.m.f. = solid oxide galvanic cell method, DSC = Differential Scanning Calorimetry, SC = Solution Calorimetry, E = estimated, CV = Calvet Calorimetry, M = manometry, C = compilation.

^a Calculated in this study from [10].

^b Given in Ref. [11].

^c Calculated in this study from [22].

Ba₃UO₆(s) [24] in a different series. In the former series, addition of UO₃(s) increases the $\Delta_f H_m^{\circ}(298.15\text{K})/\text{g}$ value and in the latter series addition of BaO(s) decreases $\Delta_f H_m^{\circ}(298.15\text{K})/\text{g}$ value. This observation also leads to a conclusion that BaO(s) stabilizes the barium uranates more than UO₃(s).

While plotting $\Delta_f H_m^{\circ}(298.15\text{K})$ as a function of Ba/U, Cordfunke et al. [26] observed $\Delta_f H_m^{\circ}(298.15\text{K})$ of $\text{Ba}_{1+y}\text{UO}_{3+x}$ and Ba₃UO₆(s) are on the same line as $\text{BaUO}_3\text{--Ba}_{1+y}\text{UO}_{3+x}\text{--Ba}_3\text{UO}_6$ belongs to perovskite series. In contrast, enthalpy of formation of Ba₂U₂O₇(s) does not fall on the line as crystal structure of Ba_{1+y}UO_{3+x} is different from Ba₂U₂O₇(s).

The stability of compounds in Ba-U-O system is poorly known [27]. The oxygen and barium potential diagrams for Ba-U-O system have been calculated using FactSage programme [28] and are shown in Figs. 7–9. Fig. 7 shows that BaUO₃(s) coexists with UO₂(s) as well as with BaO(s) whereas Ba₃UO₆(s) with BaO(s). Ba₃U₂O₈(s), Ba₂U₂O₇(s), Ba₂U₃O₁₁(s) and BaUO₄(s) coexist with UO₂(s) whereas BaU₂O₇(s) with U₃O₈(s) and BaU_{6,24}O_{19,7}(s) with UO₃(s). Fig. 8 shows that BaUO₃(s) is stable above barium potential -225 kJ mol^{-1} and Ba₃UO₆(s) in the range of -572 to -225 kJ mol^{-1} . Ba₃U₂O₈(s) is stable in a limited barium potential range that is -225 to -209 kJ mol^{-1} . BaUO₄(s) is stable in the barium potential range -600 to -510 kJ mol^{-1} . BaU₂O₇(s) and Ba₂U₃O₁₁(s) are stable below -600 kJ mol^{-1} and BaU_{6,24}O_{19,7}(s) is stable at lowest barium potential of -823 kJ mol^{-1} . UO₃(s) is stable at very low barium activity. Adamson et al. [29] reported the oxygen potential for LWR fuel to be between -550 and -450 kJ mol^{-1} . Minato et al. [30] calculated the behavior of fission products in irradiated triso-coated UO₂(s) and given a plot for equilibrium vapor pressures of the species containing barium and strontium in the fuel. Cordfunke and Ijdo [12] calculated Ba(g) over UO₂(s) at 1300 K to be around 10^{-13} kPa. In this study, the oxygen and barium potential of fuel are taken as -500 ± 50 and $-200 \pm 50\text{ kJ mol}^{-1}$, respectively, to predict the form in which the barium compounds may be present in the fuel. Figs. 7 and 8

show that BaUO₃(s), Ba₃U₂O₈(s), Ba₂U₂O₇(s) or Ba₃UO₆(s) will be possible. From these figures it is evident that stability region of Ba₃U₂O₈(s) and Ba₂U₂O₇(s) are limited. Hence, either BaUO₃(s) or Ba₃UO₆(s) will be formed, depending on the oxygen and barium pressures in the fuel element. As the BaUO₃(s) coexists with UO₂(s) and Ba₃UO₆(s) with BaO(s), BaUO₃(s) may be formed in the UO₂(s) matrix. At 1600 K, BaO(g) pressure is more than 10^{-7} kPa [30], hence there is a possibility of precipitation of BaO(s) and formation of Ba₃UO₆(s) in the cooler zone of fuel. Using X-ray microanalysis of highly irradiated fuel, Kleykamp et al. [31] showed the presence of BaUO₃(s) in grey phase. Hence, BaUO₃(s) will be stable under the reactor conditions.

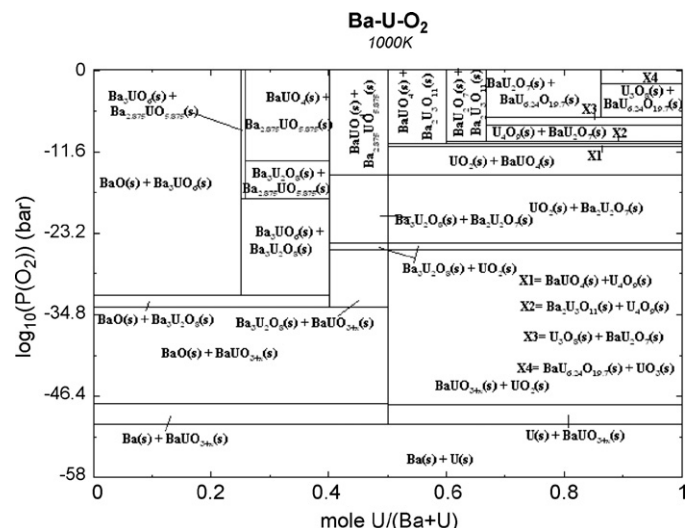


Fig. 7. Oxygen potential diagram for Ba-U-O system at 1000 K.

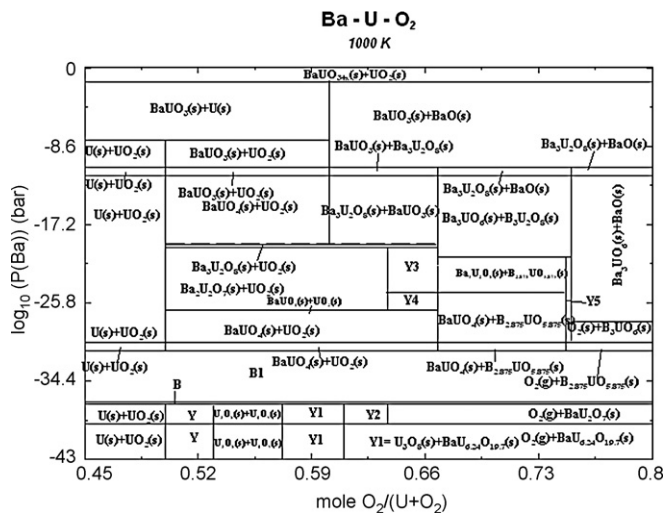


Fig. 8. Barium potential diagram for Ba-U-O system at 1000 K. $\text{BaUO}_{3+x}(\text{s})$ is a non-stoichiometric compound with distorted perovskite structure. The equilibrium phase fields: $\text{Y} = \text{UO}_2(\text{s}) + \text{U}_4\text{O}_9(\text{s})$, $\text{Y1} = \text{U}_3\text{O}_8(\text{s}) + \text{BaU}_{6.24}\text{O}_{19.7}(\text{s})$, $\text{Y2} = \text{BaU}_2\text{O}_7(\text{s}) + \text{BaU}_{6.24}\text{O}_{19.7}(\text{s})$ and $\text{Y3} = \text{Ba}_2\text{U}_2\text{O}_7(\text{s}) + \text{Ba}_3\text{U}_2\text{O}_8(\text{s})$, $\text{Y4} = \text{Ba}_2\text{U}_2\text{O}_7(\text{s}) + \text{BaUO}_4(\text{s})$, $\text{Y5} = \text{Ba}_{2.875}\text{UO}_{5.875}(\text{s}) + \text{BaUO}_4(\text{s})$ and $\text{Y6} = \text{Ba}_{2.875}\text{UO}_{5.875}(\text{s}) + \text{Ba}_3\text{UO}_6(\text{s})$.

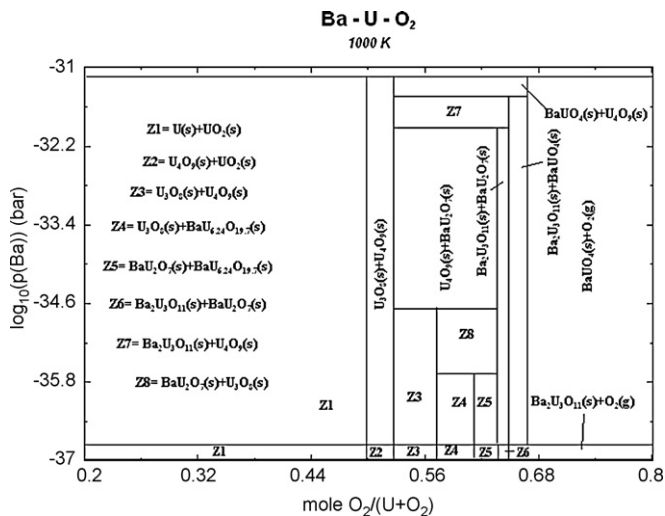


Fig. 9. The B and B1 portions of Fig. 8.

5. Conclusion

The standard molar Gibbs energy of formation of $\text{Ba}_{2.875}\text{UO}_{5.875}(\text{s})$ has been measured for the first time. $\Delta_f H_m^\circ$

($\text{Ba}_{2.875}\text{UO}_{5.875}(\text{s})$, s , 298.15 K) value calculated from third law is $-3137.7 \pm 4 \text{ kJ mol}^{-1}$. $\Delta_f G_m^\circ(T)$ per mole of $\text{O}_2(\text{g})$ data as a function of temperature have been plotted for various barium uranates in BaO-UO₃ system. It has been concluded from the plot that higher mole fraction of BaO(s) stabilizes the barium uranates. The oxygen and barium potential diagrams for Ba-U-O system have been calculated. The calculations show that $\text{BaUO}_3(\text{s})$ will be formed in the $\text{UO}_2(\text{s})$ matrix.

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